

TRANSVERSE RESISTIVE WALL IMPEDANCE FOR SIS100 (AT GSI) AND LHC COLLIMATOR

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**Slava is writing a Technical Proposal:
“The Transverse Damping Systems for SIS100&SIS300”**

◆ **Comparison between Zotter2005 and Balbekov1985***

* V.I. Balbekov, Space Charged Effects in UNK, in The IX All Union Conference on Particle Accelerators, JINR, Dubna, vol. 2, p. 360, 1985 (in Russian)

Beam and machine parameters for SIS100

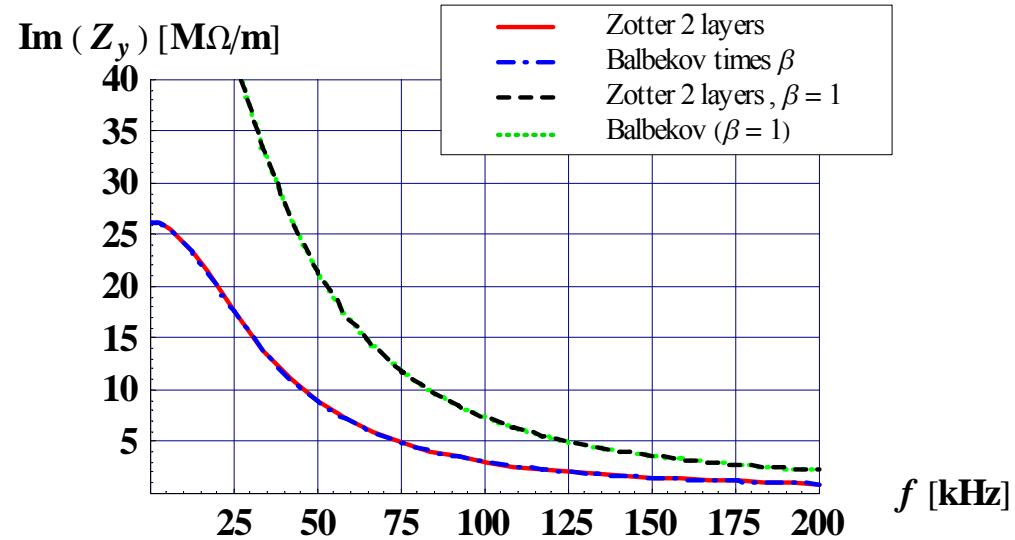
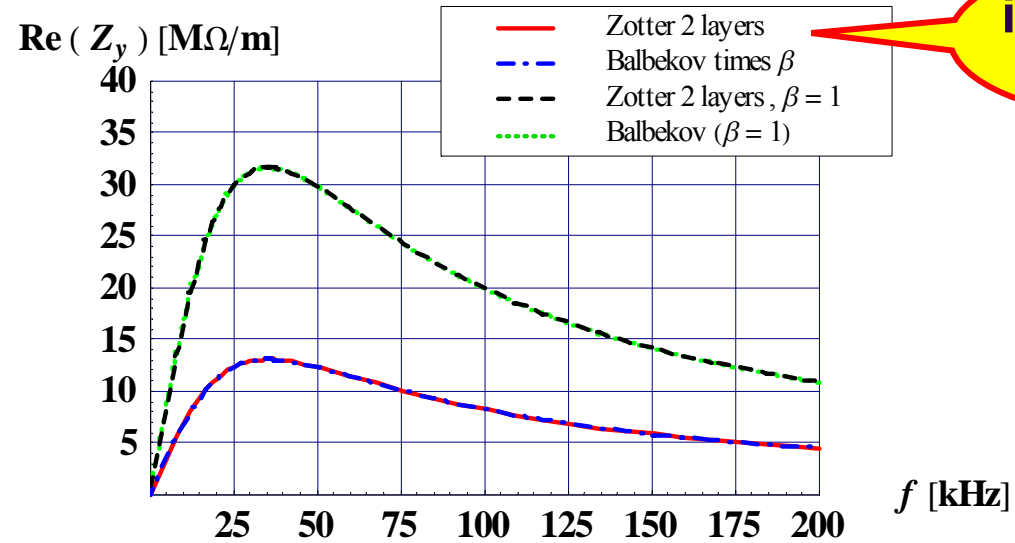
⇒ Computation for $^{238}\text{U}^{28+}$ at injection, assuming (first) a round pipe with radius 32 mm (=vertical half axis)

Machine circumference [m]	1083.6
Beam rigidity [Tm]	12
β	0.413
γ	1.098
f_{rev} [kHz]	114.4
ρ [Ωm] \Rightarrow SS	$9 \cdot 10^{-7}$
Vacuum chamber thickness [mm]	0.2 or 0.3
Horizontal half axis [mm]	32 (65 normally)
Vertical half axis [mm]	32

Vacuum chamber thickness = **0.2 mm**

... assuming the whole machine circumference with the same resistivity

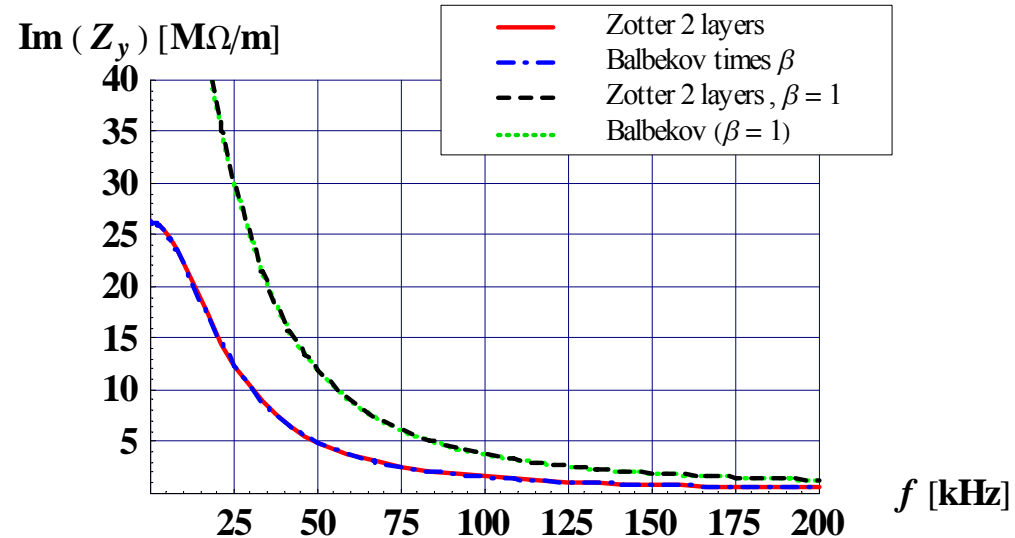
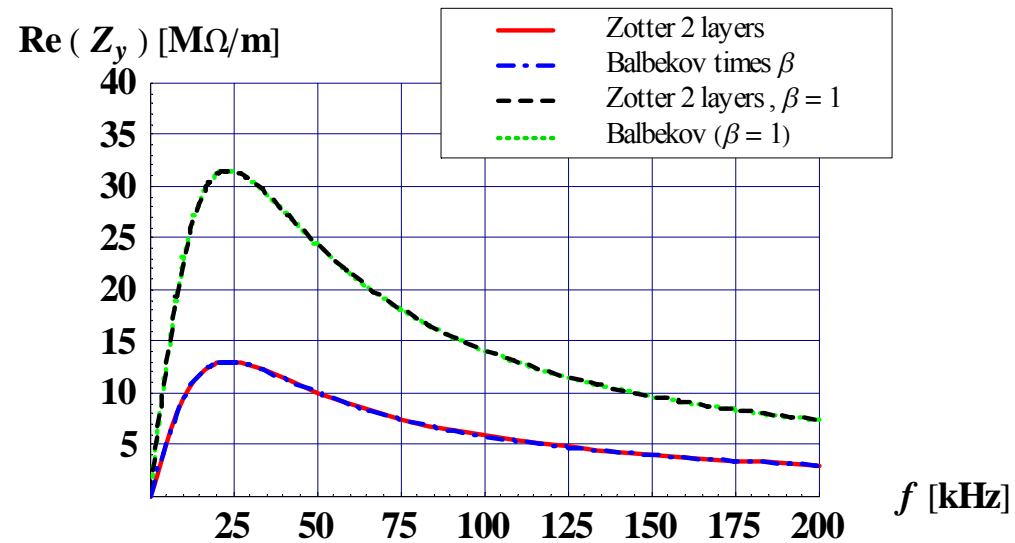
Skin depth = 0.2 mm
 $\Leftrightarrow f = 5.7 \text{ MHz}$



Vacuum chamber
thickness = **0.3 mm**

... assuming the whole
machine circumference
with the same resistivity

Skin depth = 0.3 mm
 $\Leftrightarrow f = 2.5 \text{ MHz}$



LHC graphite collimator

$$L = 1 \text{ m}$$

$$b = 2 \text{ mm (half gap)}$$

$$\rho_C = 10 \mu\Omega\text{m}$$

$$d_C = 2.5 \text{ cm}$$

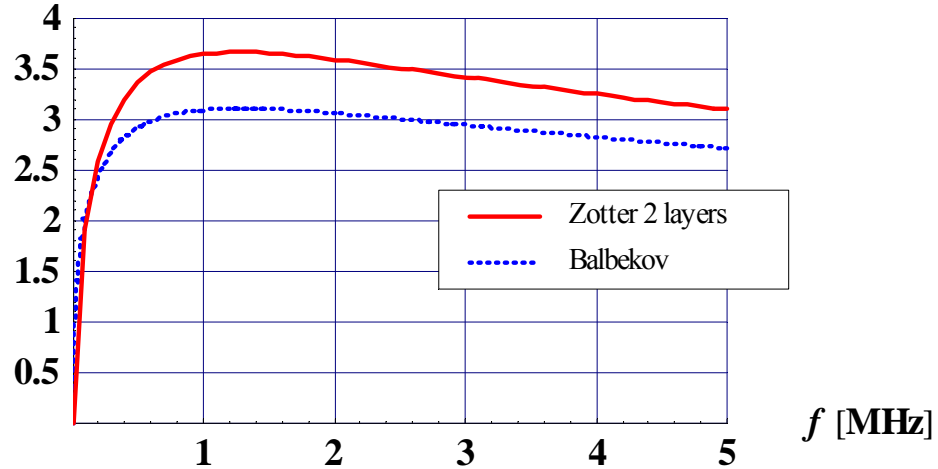
$$\gamma = 7462.69$$

$$\beta = 1$$

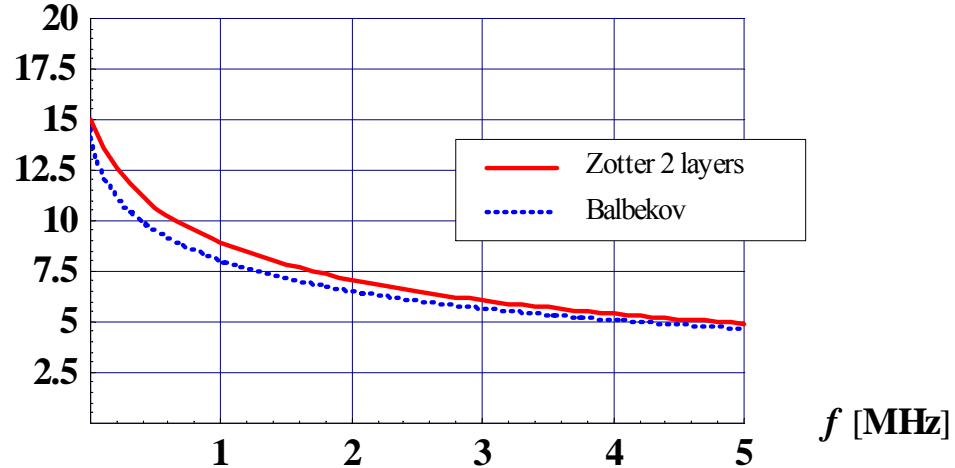
$$\text{Skin depth} = 2.5 \text{ cm}$$

$$\Leftrightarrow f = 4 \text{ kHz}$$

$\text{Re}(Z_y)$ [$\text{M}\Omega/\text{m}$]



$\text{Im}(Z_y)$ [$\text{M}\Omega/\text{m}$]



LHC graphite collimator

$$L = 1 \text{ m}$$

$$b = 2 \text{ mm (half gap)}$$

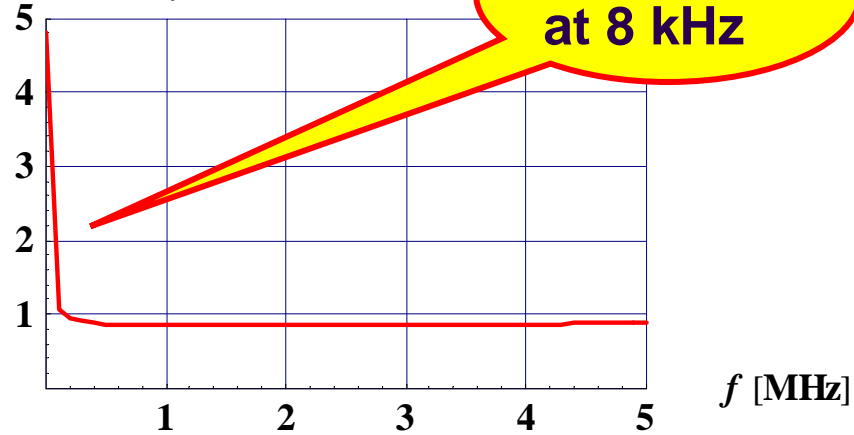
$$\rho_C = 10 \mu\Omega\text{m}$$

$$d_C = 2.5 \text{ cm}$$

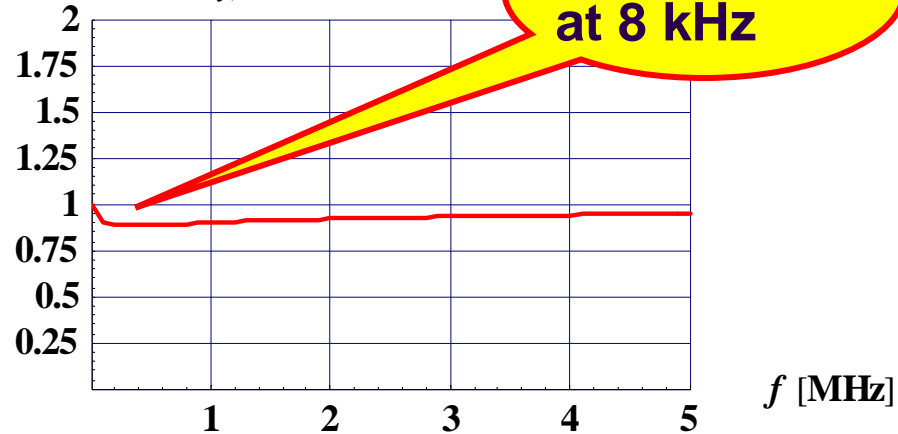
$$\gamma = 7462.69$$

$$\beta = 1$$

$\text{Re} (Z_{y, \text{Balbekov}}) / \text{Re} (Z_{y, \text{Zotter}})$



$\text{Im} (Z_{y, \text{Balbekov}}) / \text{Im} (Z_{y, \text{Zotter}})$



APPENDIX 1: BALBEKOV'S FORMULA FOR A ROUND PIPE

$$Z_y = \frac{j L Z_0}{2 \pi b^2} \times \frac{1}{1 + \frac{b}{(1-j)\delta \coth \left[(1+j) \frac{d}{\delta} \right]}}$$

“Inductive-bypass” effect due to this term (\Rightarrow 2 impedances in // as Vos2003)

where

L = Length of the object

$Z_0 = 120 \pi$

b = Half gap

δ = Skin depth

d = Thickness of the vacuum chamber

**APPENDIX 2: Draft paper
 “Damping of Transverse
 Instabilities for Coasting
 Beams” by V. Kornilov,
 O. Boine-Frankenheim,
 I. Hofmann and B. Doliwa
 ⇒ Given to me (for
 comments) by Slava**

No “inductive-bypass” term

3 Impedances

The transverse impedance due to the space charges (sc) we evaluate using

$$Z_{sc}^{\perp} = iZ_0 \frac{R}{\beta\gamma^2} \left[\frac{1}{a^2} - \frac{1}{b^2} \right], \quad (29)$$

in which we take into account the elliptic cross-sections replacing the radii as $2a^2 \rightarrow R \left(\frac{\epsilon_{v,h}}{Q_{v,h}} + \sqrt{\frac{\epsilon_v \epsilon_h}{Q_v Q_h}} \right)$.

The impedance stemming from a resistive wall with thickness d_{pipe} we estimate [2] as

$$Z_{rw}^{\perp} = \frac{2\beta c}{b^2 \Omega} Z_{rw}^{\parallel} = (1-i)Z_0 \frac{R\beta \delta_{\text{skin}}}{b^3} \coth \left\{ \frac{\Omega}{\beta c} \sqrt{\frac{1}{\gamma^2} - i \frac{4\pi\sigma\beta^2}{\Omega}} d_{\text{pipe}} \right\} \quad (30)$$

($\delta_{\text{skin}} = c/\sqrt{2\pi\sigma\Omega}$, $Z_0 = 4\pi/c$). Figure 4 shows this impedance in its dependencies on the coherent frequency Ω (left-hand side) and on the wall thickness d_{pipe} (right-hand side). The parameters taken correspond to a U^{28+} coasting beam at the injection energy, see Table 3 and Table 4 in the Appendix. The right-hand side plot is made for the frequency 156 kHz, the corresponding skin length is $\delta_{\text{skin}} = 1.1$ mm. For the left-hand side plot, the skin length

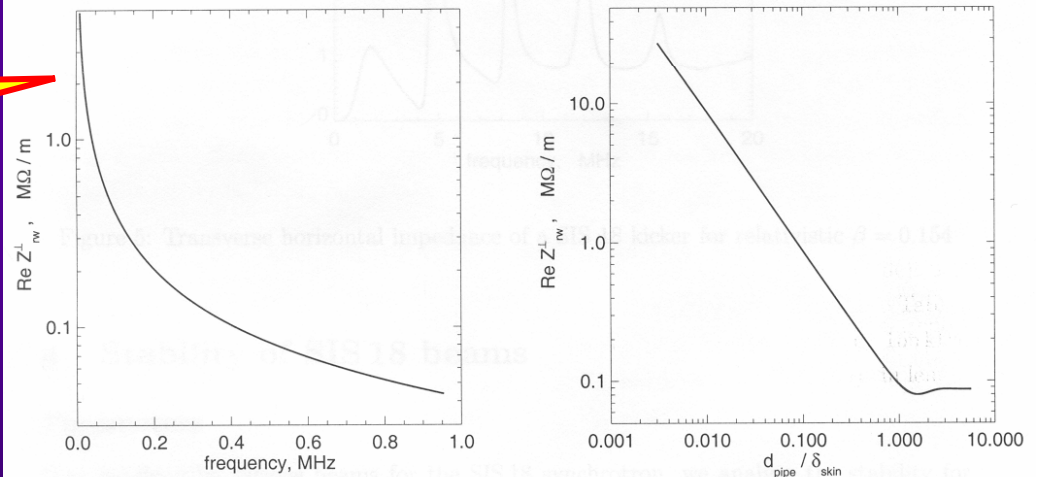


Figure 4: Transverse resistive wall impedance [Eq. (30)] as a function of the frequency (left) and of the wall thickness (right). Note the logarithmic scale for Z_{rw}^{\perp} and d_{pipe} .

is equal to $\delta_{\text{skin}} = 0.3$ mm at the frequency 1.9 MHz, i.e. this is the thin-wall regime for such a pipe.